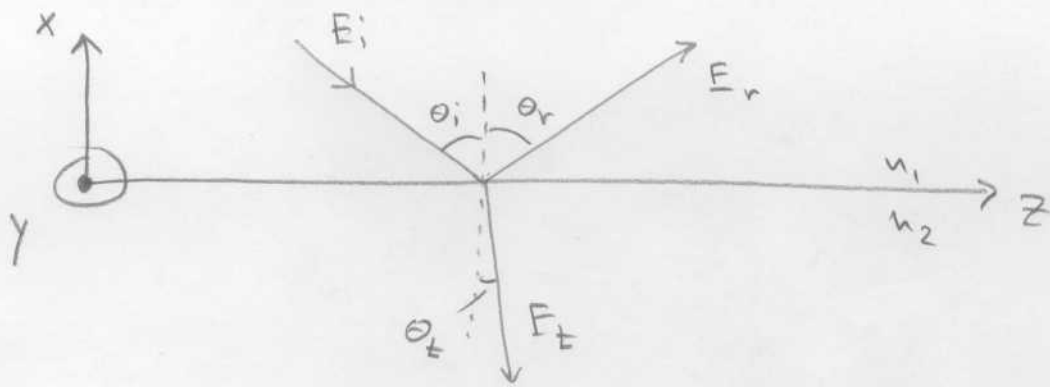


FRESNELS FORMLER



$$\begin{cases} E_i = E_{i0} \cdot e^{i(\vec{k} \cdot \vec{r} - \omega t)} \\ E_r = E_{r0} \cdot e^{i(\vec{k}_r \cdot \vec{r} - \omega_r t)} \\ E_t = E_{t0} \cdot e^{i(\vec{k}_t \cdot \vec{r} - \omega_t t)} \end{cases}$$

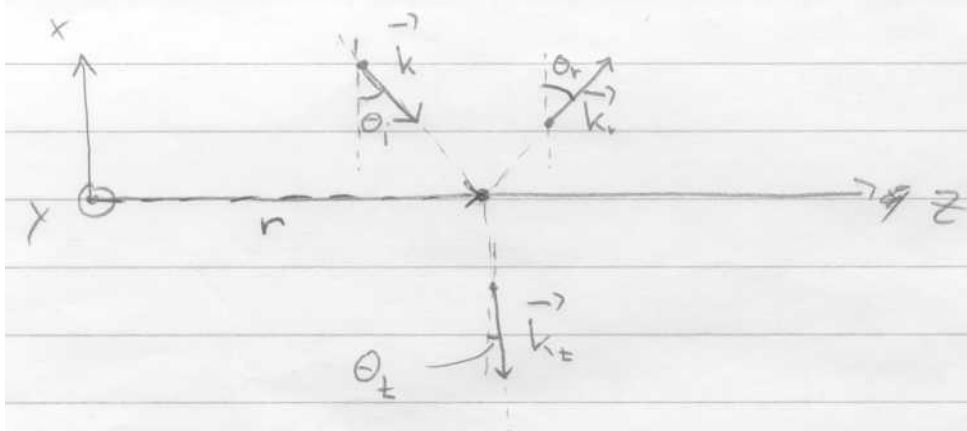
Vid infallspunkten måste det valda ett visst förhållande mellan E_i , E_r och E_t som är oberoende av $\vec{r}$ och t .

$\Rightarrow$ Faserna måste vara lika!!

$$(\vec{k} \cdot \vec{r} - \omega t) = (\vec{k}_r \cdot \vec{r} - \omega_r t) = (\vec{k}_t \cdot \vec{r} - \omega_t t)$$

$$\text{t.ex. } \vec{r} = \vec{0} \Rightarrow \omega = \omega_r = \omega_t$$

$$\text{t.ex. } t = 0 \Rightarrow \vec{k} \cdot \vec{r} = \vec{k}_r \cdot \vec{r} = \vec{k}_t \cdot \vec{r}$$



$\vec{k}_r$ och $\vec{k}_t$ ligger också i infallplanet

$$\Rightarrow k \cdot \sin \theta_i = k_r \cdot \sin \theta_r$$

$$k = \frac{2\pi}{\lambda} \cdot n_1, \quad k_r = \frac{2\pi}{\lambda} \cdot n_1 \Rightarrow k_r = k$$

$$\Rightarrow \theta_r = \theta_i; \text{ Refl. lagar}$$

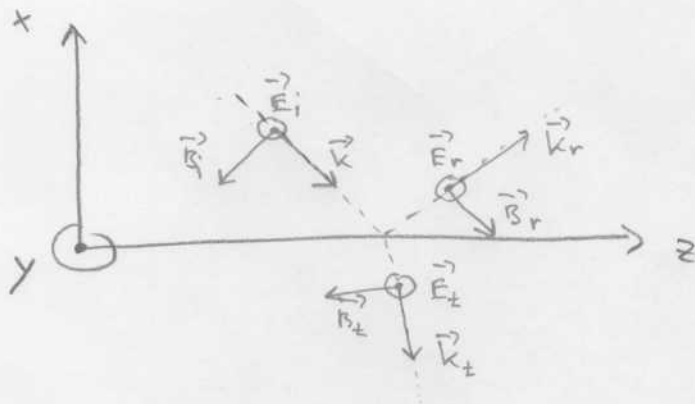
$$k \cdot \sin \theta_i = k \cdot \sin \theta_t$$

$$k_t = \frac{2\pi}{\lambda} \cdot n_2, \quad \frac{2\pi}{\lambda} n_1 \sin \theta_i = \frac{2\pi}{\lambda} \cdot n_2 \sin \theta_t$$

$$\Rightarrow n_1 \cdot \sin \theta_i = n_2 \cdot \sin \theta_t; \text{ Snell}$$

Amplitud förhållanden

① pol. $\perp$ mot infallsplanet:



E-fältet transversellt mot infallsplanet

"TE-MOD" ("⊥-komp.")

Maxwell $\Rightarrow$ komp. av $\vec{E}$ och $\vec{B}$ som är
// med ytan är kontinuerliga

$$\begin{cases} E + E_r = E_t \\ -B \cos \theta_i + B_r \cos \theta_i = -B_t \cos \theta_t \end{cases}$$

$$E = \frac{c}{u} B \quad \Rightarrow \quad B = \frac{u}{c} E$$

$$\begin{cases} E + E_r = E_t \\ u_1 E \cos \theta_i - u_1 E_r \cos \theta_i = u_2 E_t \cos \theta_t \end{cases}$$

$$\Rightarrow E u_1 \cos \theta_i - E_r u_1 \cos \theta_i = E u_2 \cos \theta_t + E_r u_2 \cos \theta_t$$

$$E (u_1 \cos \theta_i - u_2 \cos \theta_t) = E_r (u_2 \cos \theta_t + u_1 \cos \theta_i)$$

$$r_{\perp} = \frac{E_r}{E} = \frac{n_1 \cos \theta_i - n_2 \cos \theta_t}{n_1 \cos \theta_i + n_2 \cos \theta_t} =$$

$$= \frac{\cos \theta_i - \frac{n_2}{n_1} \cos \theta_t}{\cos \theta_i + \frac{n_2}{n_1} \cos \theta_t} = \frac{\cos \theta_i - \frac{\sin \theta_i}{\sin \theta_t} \cos \theta_t}{\cos \theta_i + \frac{\sin \theta_i}{\sin \theta_t} \cos \theta_t} =$$

$$= \frac{\cos \theta_i \sin \theta_t - \sin \theta_i \cos \theta_t}{\cos \theta_i \sin \theta_t + \sin \theta_i \cos \theta_t} =$$

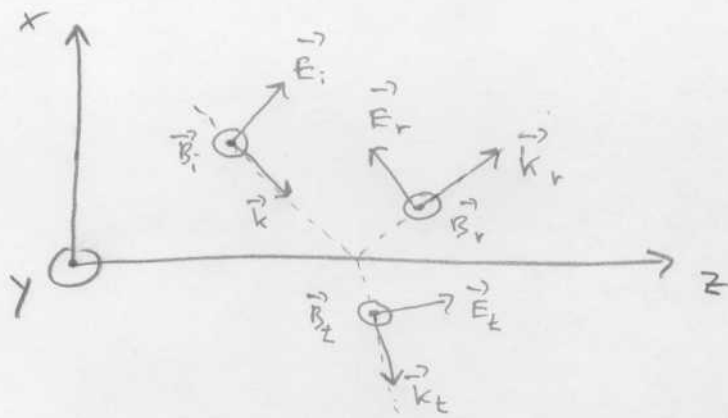
$$= - \frac{\sin(\theta_i - \theta_t)}{\sin(\theta_i + \theta_t)}$$

E *

$$E + r_{\perp} = t_{\perp} E \quad \Rightarrow \quad t_{\perp} = r_{\perp} + 1 = \frac{E_t}{E}$$

$$\Rightarrow \quad t_{\perp} = \frac{2 \cos \theta_i \sin \theta_t}{\sin(\theta_i + \theta_t)}$$

② pol. // med infallsplanet



B-fältet transversellt mot infallsplanet

"TM-MOD" ("// - komp.")

Maxwell (p.s.s. som förut)

$$\begin{cases} B + B_r = B_t \\ E \cos \theta_i - E_r \cos \theta_r = E_t \cos \theta_t \end{cases}$$

----- Analog härledning -----

$$\Rightarrow r_{||} \text{ och } t_{||}$$

TE:

$$r_{\perp} = - \frac{\sin(\theta_i - \theta_t)}{\sin(\theta_i + \theta_t)}$$

$$t_{\perp} = \frac{2 \cos \theta_i \sin \theta_t}{\sin(\theta_i + \theta_t)}$$

TM:

$$r_{\parallel} = \frac{\tan(\theta_i - \theta_t)}{\tan(\theta_i + \theta_t)}$$

$$t_{\parallel} = \frac{2 \cos \theta_i \sin \theta_t}{\sin(\theta_i + \theta_t) \cos(\theta_i - \theta_t)}$$

r : reflections coeff

t : transmissioes coeff

Ref. och Trans IRRADIANS

~~OH 18-1~~
OH 11-2

Energiprincipen: $P_i = P_r + P_t$

Antag homogen infördelning:

$$I_i A_i = I_r A_r + I_t A_t$$

$$I_i A \cos \theta_i = I_r A \cos \theta_r + I_t A \cos \theta_t$$

$$\left\{ I = \frac{1}{2} \epsilon_0 \epsilon_r \frac{c}{n} E_0^2 = \frac{1}{2} \epsilon_0 n^2 \frac{c}{n} E_0^2 = \frac{1}{2} \epsilon_0 n c E_0^2 \right\}$$

$$\Rightarrow n_1 \cos \theta_i E_{0i}^2 = n_1 \cos \theta_r E_{0r}^2 + n_2 \cos \theta_t E_{0t}^2$$

$$E_{0i}^2 = E_{0r}^2 + \frac{n_2}{n_1} \frac{\cos \theta_t}{\cos \theta_i} E_{0t}^2$$

$$1 = r^2 + \frac{n_2}{n_1} \frac{\cos \theta_t}{\cos \theta_i} t^2$$

Reflektans irradians: $I_r = R \cdot I_i$

$$R = r^2$$

Transmittans irradians: $I_t = T \cdot I_i$

$$T = \frac{n_2}{n_1} \frac{\cos \theta_t}{\cos \theta_i} t^2$$

$$1 = R + T$$

$\left\{ \begin{array}{l} R: \text{"Reflektans"} \\ T: \text{"Transmittans"} \end{array} \right.$

R och T vid ext. resp. int. refl.

① Extern refl. ($n_1 < n_2$)

$$\begin{cases} R = r^2 \\ T = \frac{n_2}{n_1} \frac{\cos \theta_t}{\cos \theta_i} t^2 \end{cases} \text{ + Fresnels Form. + Snell}$$

$\Rightarrow$

~~OH 18-2~~
OH 11-3

$\{ n_1 = 1, n_2 = 1.5 \text{ i exempel} \}$

$$\theta_i = 0 \Rightarrow R_{\perp} = R_{\parallel} = 0.04$$

$$\theta_i \rightarrow 90^\circ \Rightarrow R_{\perp}, R_{\parallel} \rightarrow 1$$

$$\theta_i = \theta_B \Rightarrow R_{\parallel} = 0, R_{\perp} \approx 0.15 \\ = 56^\circ$$

(Brewster-vinkel)

② Intern Refl. ($n_1 > n_2$)

~~OH 18-3~~
OH 11-4

$$\theta_i = 0 \Rightarrow R_{\parallel} = R_{\perp} = 0.04$$

$$\theta_i \rightarrow \theta_c \Rightarrow R_{\perp}, R_{\parallel} \rightarrow 1 \\ = 46^\circ$$

(kritisk vinkel för total refl.)

$$\theta_i = \theta_B = 34^\circ \Rightarrow R_{\parallel} = 0, R_{\perp} \approx 0.15$$

$$\theta_i > \theta_c \Rightarrow r_{\perp} \text{ och } r_{\parallel} \text{ kompletta}$$

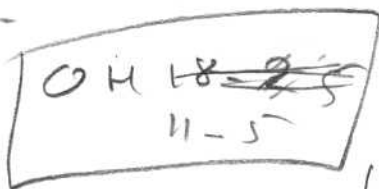
$$|r_{\perp}| = |r_{\parallel}| = 1 \Rightarrow \text{Total refl.}$$

Fasshift vid refl.

negativt värde ρ_D $r \Rightarrow$ fasshift med π

$$\left\{ \begin{aligned} E_r &= -|r| E_i = \cos \pi \cdot |r| E_i = (\cos \pi + i \sin \pi) |r| E_i = \\ &= e^{i\pi} |r| E_{i0} e^{i(\vec{k} \cdot \vec{r} - \omega t)} = |r| \cdot E_{i0} e^{i(\vec{k} \cdot \vec{r} - \omega t + \pi)} \end{aligned} \right\}$$

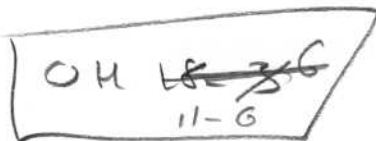
Ext. refl.



fasshift med π då

$$\left\{ \begin{aligned} \text{TE-mod}(\perp) &: \text{alla } \theta_i \\ \text{TM-mod}(\parallel) &: \theta_i > \theta_B \end{aligned} \right.$$

Int. refl.

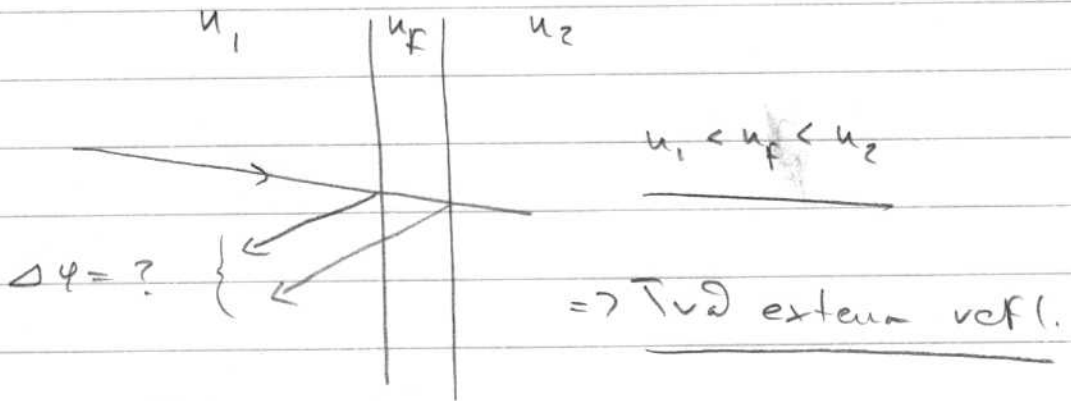


fasshift med π då

$$\left\{ \begin{aligned} \text{TE-mod}(\perp) &: \text{alltid} \text{ c.s.d.} \text{ linse } \theta_i < \theta_c \\ \text{TM-mod}(\parallel) &: \theta_i < \theta_B \end{aligned} \right.$$

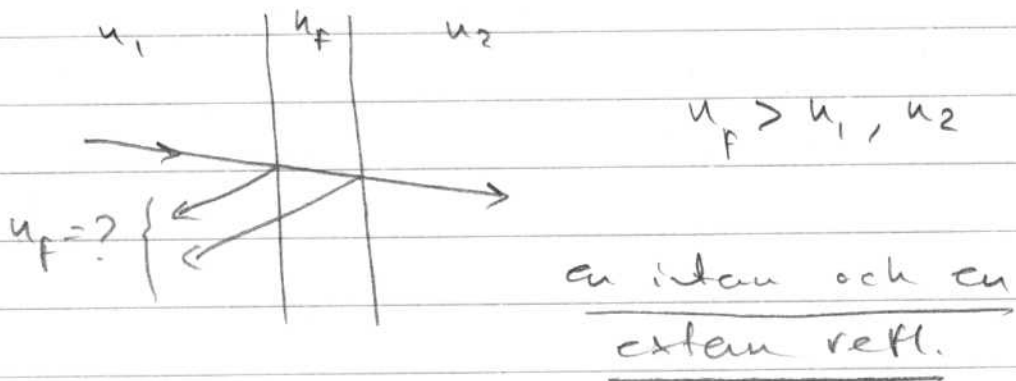
Hur blir fasshiftet mellan två komponenter som reflekteras i gräns resp. bakre ytan av ett tunt skikt?

1)



1. Eftersom båda refl. är av samma typ så blir $\Delta\phi = 0$

2)



2a: TE-mod ($\perp$)

Extern refl har alltid ett fasshift på π
intern " " " " " " " " " " " "

$$\Rightarrow \Delta\phi = \pi$$

2b: TM-mid (

$\theta_i < \theta_B$: ext. refl $\rightarrow \varphi = 0$

int. refl $\rightarrow \varphi = \pi$

$\theta_i > \theta_B$: ext. refl $\rightarrow \varphi = \pi$

int. refl $\rightarrow \varphi = 0$

$\Rightarrow \Delta\varphi = \pi$ alltid

OH 11.7

Slutsats:

Stenbriannärsigt säga man allt det
sker en fasshift vid extan, men inte
vid intan refl.

Inte helt sant, men det leder oftast
till rätt slutsats

Totalreflektion

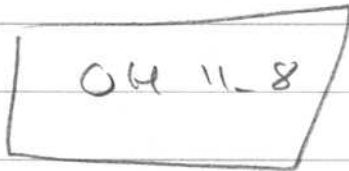
$$\varphi = ?$$

inlein refli., $\theta_i > \theta_c$

$$\Rightarrow r_{\perp} = e^{i\varphi_{\perp}}, \quad r_{\parallel} = e^{i\varphi_{\parallel}}$$

(komplex!)

Häledning av $\varphi_{\perp}$ och $\varphi_{\parallel}$ ger

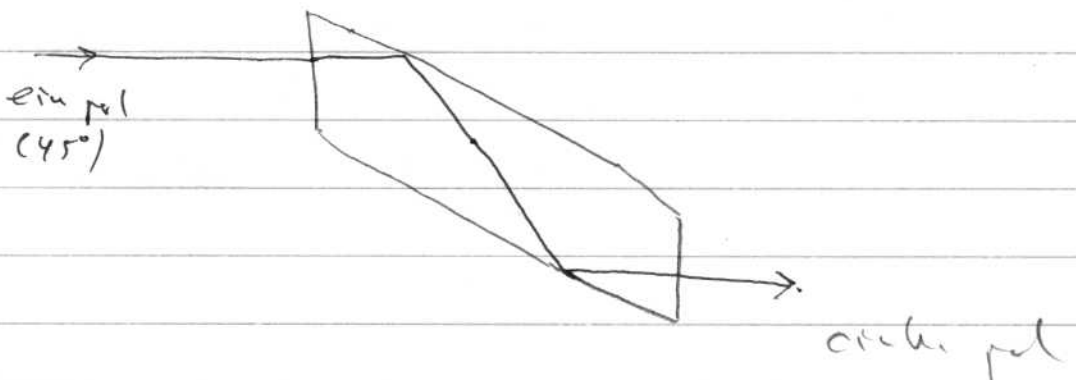


$$\text{Ex: } \theta_i \approx 50^\circ \Rightarrow \Delta\varphi = \varphi_{\parallel} - \varphi_{\perp} = 45^\circ$$

$\Rightarrow$ två successiva refli. kan ändra
den relativa fasen med 90°

$\Rightarrow$ vinkelår pol!

Fisshelvan b



Speziell, normaler Fall ($\theta_i = \theta_L = 0$)

$$\Rightarrow r_{\perp} = - \frac{\sin(\theta_i - \theta_L)}{\sin(\theta_i + \theta_L)} = - \frac{\theta_i - \theta_L}{\theta_i + \theta_L} =$$

$$= - \frac{\theta_i - \frac{n_1}{n_2} \theta_i}{\theta_i + \frac{n_1}{n_2} \theta_i} = - \frac{n_2 - n_1}{n_2 + n_1} = \frac{n_1 - n_2}{n_1 + n_2}$$

normaler Fall:

$$\boxed{\begin{aligned} r_{\perp} &= \frac{n_1 - n_2}{n_1 + n_2} \\ r_{\parallel} &= \frac{n_2 - n_1}{n_1 + n_2} \end{aligned}}$$

$$|r_{\perp}| = |r_{\parallel}| \Rightarrow R_{\perp} = R_{\parallel}$$